thread milling cutter of stock size can be used. This cutter will have a 1 in. hole diameter and an outside diameter of 2 % in. The cutter is swiveled to the angle of 2° 52′, and is then centered on the worm blank.

## MILLING A HIGH SPEED CARBIDE CUTTER BODY

Carbide face mill cutters differ greatly in diameter, number of teeth, and rake angles. The following specifications are used as a typical example:

- 1. Diameter of Cutter Body = 8"
- 2. Number of Teeth = 10
- 3. Axial Rake Angle = -10°
- 4. Radial Rake Angle = -10°
- 5. Carbide Tooth Thickness =  $\frac{3}{16}$ " Before milling, the following lathe operations should be completed:
- 1. Turn the periphery to size.
- 2. Face both sides parallel and square with periphery.

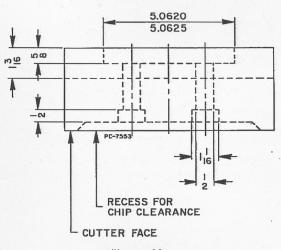


Figure 49
Dimensions of a
Typical Cutter Body

- 3. Bore the whole which fits over the milling machine spindle nose to a depth of  $\frac{5}{8}$ " and 5.0620"-5.0625" diameter, and square with the face. (Figure 49).
- 4. Turn a recess in the face of the cutter body to allow for chips.

Mill Driving Key Slots (Figure 49). This operation is not completed with the aid of the Dividing Head, but we have included the details for sake of completeness in machining the cutter body.

- 1. Clamp the cutter body face down on the table of the machine and fasten an arbor, fitted with either an inter-locking or stagger tooth cutter of the correct thickness, in the machine spindle. Lock arbor support and overarm in position. Select correct cutter speed and feed.
- 2. Accurately measure the diameter of the cutter body with a micrometer. Adjust the knee, saddle, and table to bring the side of the cutter tangent to the periphery of the cutter body.
- 3. Start the spindle and hold a thin piece of paper between rotating cutter and the periphery of the cutter body. Move saddle in slowly until the paper is pulled between the cutter and body.
- 4. Lower the knee and move the saddle in ½ the diameter of the cutter body plus ½ the thickness of the cutter plus the thickness of the paper. Start the spindle and raise the knee until the rotating cutter contacts the top of the cutter body. Move the table to the right, raise the knee 1¾6″, and mill the driving key slot.

### CINCINNATI UNIVERSAL DIVIDING HEADS

### Mill Carbide Insert Seats.

- 1. Mount Dividing Head, with four-jaw chuck, in rear T-slot (slot nearest column) of machine. Fasten a 1" four flute end mill, together with a suitable adaptor, in machine spindle. Select correct speed and feed.
- 2. Free the Dividing Head spindle by disengaging the worm from worm wheel. Grip the cutter body with Dividing Head chuck by expanding the jaws in the 5½6" bored hole (Figure 49). Protect the bored surface from the hardened steel chuck jaws with shim stock.

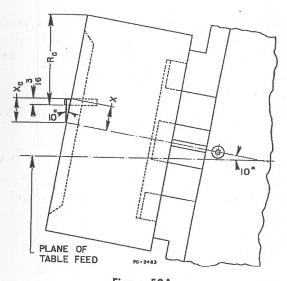


Figure 50A
Sketch Showing Calculation
of Distance to Raise Knee

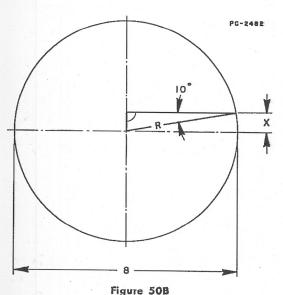
Test the periphery and face of cutter body with a dial indicator and then eliminate eccentricity by shifting the chuck jaws. When cutter body runs concentric, engage worm with worm wheel.

- 3. Set the Dividing Head for the axial rake angle of minus 10°. This is accomplished by swiveling the Dividing Head up 10° from the horizontal (Figure 50A). The vernier scale on the Dividing Head may be used to accurately adjust the head.
- 4. Set the cutter off-center for the radial rake angle of minus 10°. The amount of off-set (Figure 50B) and distance to raise the knee (Figure 50A) can be calculated in the following manner:

Sine 
$$10^{\circ} = \frac{X}{r}$$
 $X = r \text{ Sine } 10^{\circ}$ 
 $X = 4 \times .17365$ 
 $X = .6946$ 

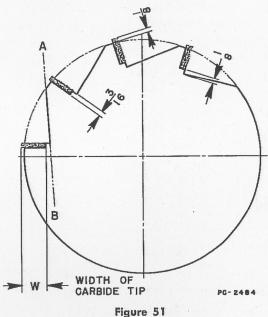
Now calculate the corrected X dimension (Xc) and the correct R dimension (Rc) (Figure 50A).

$$\begin{array}{c} \text{Cos } 10^{\circ} = \frac{\text{Xc}}{\text{X}} \\ \text{Xc} = \text{X Cos } 10^{\circ} \\ \text{Xc} = .98481 \times .6946 \\ \text{Xc} = .682 \\ \text{Cos } 10^{\circ} = \frac{\text{Rc} \times (\text{Xc} - \text{tooth thickness})}{4} \\ \text{Cos. } .98481 = \frac{\text{Rc} + (.6820 - .1875)}{4} \\ \text{Rc} + (.6820) - .1875 = .98481 \times 4 \\ \text{Rc} + .4945 = 3.93924 \\ \text{Rc} = 3.9392 - .4945 \\ \text{Rc} = 3.444'' \end{array}$$



Sketch Showing Calculation of Amount of Offset

- 5. Start the spindle, adjust table, knee and saddle to position the rotating cutter directly above the highest point on the periphery of the cutter body. Use a piece of tissue paper for touching up. Back away the saddle and raise the knee Rc dimension.
- 6. Move in the saddle until the face of the rotating cutter contacts the periphery of the cutter body. Move the table to the right to clear the rotating cutter. Measure the width "W" of the carbide tip, (Figure 51) subtract  $\frac{1}{8}$ " and move the saddle in this amount. If the width of the carbide tip is considerably wide it may be necessary to take several cuts before the desired depth is reached.
- 7. Engage the table feed lever and mill the carbide tip seat in the cutter body. Turn the crank of the Dividing Head 4 complete turns and return the index pin to the same hole in the index plate. Repeat this operation until all ten carbide tip seats are milled.
- 8. After the last seat has been milled, lower the knee ¾16" (tooth thickness) and move the saddle in ½" (Figure 51). This is done to provide clearance for the grinding wheel when grinding the face of the carbide teeth. Engage the table feed lever and take a cut. Index and repeat this operation on the remaining seats.
- 9. The chip clearance or gullet is milled next (Figure 51). Scribe a line on the face of the cutter body from "A" to "B" (Figure 51). Position cutter body so line is square with top of table. Start spindle and mill off all the metal outside of this line. Index and repeat this operation. Remove the cutter (not the cutter body).



Cutting the Gullets

- 10. Swivel the Dividing Head spindle to a horizontal position, loosen tee-bolts, and move the Dividing Head to another part of the table. Fasten a Dividing Head angle plate, fitted with tongue strips, to table. Mount Dividing Head on angle plate so face of cutter body is facing the column.
- 11. Adjust the knee and table to position the cutter body central with the machine spindle. Fasten an indicator to the machine spindle and in contact with the work periphery. Disengage the spindle drive. Rotate the spindle by hand and watch the dial indicator as it revolves around the periphery of the cutter body. Adjust the

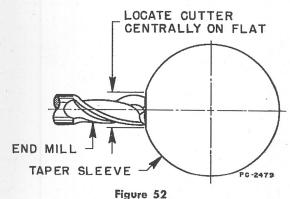
table and knee until the indicator shows zero movement during its complete revolution. Remove the dial indicator from machine spindle and engage spindle drive.

- 12. Disengage the Dividing Head worm from the worm wheel. Rotate the cutter body until the driving key slots are parallel to the machine table. Check the parallelism with an indicator on the table. Lock the Dividing Head spindle and engage the worm with the worm wheel. If the index pin in the Dividing Head crank does not fit into a hole in the index plate, release the stop which locks the index plate and rotate the plate in either direction until pin enters a hole. Relock the index plate stop and release the Dividing Head spindle lock.
- 13. Mount a suitable adaptor on the spindle nose of the machine. Fasten a  $\frac{3}{16}$ " center drill and holder in the adaptor. Select the correct spindle speed. Raise the knee 2.000" and turn the index crank 5 complete revolutions and return the pin to the same hole in the index plate. Start spindle and center drill the face of the cutter body. Turn the index crank 10 complete turns and repeat this operation. After center drilling four holes, drill completely through the cutter body with a  $\frac{21}{32}$ " drill (Figure 49). Replace the  $\frac{21}{32}$ " drill with a  $\frac{11}{16}$ " end mill and co-bore the four holes to a depth of  $\frac{1}{2}$ ". Cutter body is now complete and ready for the brazing of carbide tips.

### MILLING THE TANG AND CENTER KEY-SLOT ON A TAPER SLEEVE

Milling operations on taper sleeves and similar parts constitute a common Dividing Head setup. Nevertheless, high quality workmanship is difficult to obtain because of the small cutters required for the operation, and the large amount of metal which must be removed. The instructions given briefly outline both tang and key slot operations.

- 1. Clean milling machine table and bottoms of Dividing Head and tailstock.
- 2. Clamp Dividing Head in rear T-slot with spindle in horizontal position. Mount a test bar in spindle and check parallelism between spindle and table with a dial indicator.
- 3. Clamp tailstock to table. An aligning bar and dial indicator may be used for obtaining correct alignment between tailstock center and Dividing Head center.
- 4. Dog large end of taper sleeve and mount between centers.



Centering an End Mill

- 5. Fasten a ¼" two flute straight shank end mill into a holder and mount holder and a suitable adapter in spindle of machine. End mill must have at least 5/8" flute length. Select correct cutter speed and feed.
- 6. Lay off the 1¾<sub>16</sub>" dimension as per Figure 53A. Position table, knee, and saddle so 1¾<sub>16</sub>" dimension is directly in front of cutter. Start machine spindle and move saddle in by hand until cutter starts cutting. Center cutter with flat just milled on taper sleeve (Figure 52).
- 7. Position table so cutter is at one end of 13/16" dimension. Move saddle in by hand about .250", engage table feed and mill length of slot. Repeat until flute length is consumed. Back out saddle, turn index crank 20 turns (180°) and return pin to same hole in index plate. Repeat above milling operation until slot is through taper sleeve.

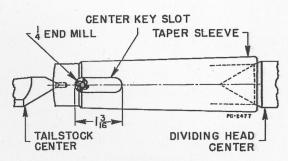


Figure 53A
Milling Center Key-Slot

- 8. Stop machine, remove two flute end mill and replace it with a 1/4" four flute straight shank end mill having a 11/4" flute length or greater.
- 9. Start machine and move saddle in until cutter extends completely through taper sleeve. Raise knee a few thousandths and take a cut. Move saddle out, return table to its start position, turn index crank 20 turns and take another cut. Measure slot with gage blocks. Raise knee ½ the difference between the gage blocks size and the size of the finished slot. Take another cut, back out saddle, and return table to start position. Turn index crank 20 turns, again move saddle in and take another cut. Measure slot, take another cut if necessary.
- 10. Turn index crank 10 turns (90°). Stop machine and replace cutter with a 5/8" four flute straight shank end mill. It will also be necessary to change the cutter holder, feed and speed.
- 11. Start machine spindle and position table, knee, and saddle so cutter is directly over small end of taper sleeve.

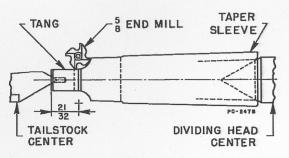


Figure 53B
Milling the Tang

12. Raise knee until cutter contacts work, move table to right and further raise knee about .125". Lay off the <sup>21</sup>/<sub>32</sub>" dimension, Figure 53B. Engage table feed and take first cut. Stop machine, move table to right, and turn index crank 20 turns (180°). Start machine and take a second cut. Measure thickness of tang with micrometer and repeat above milling operation until correct thickness of tang is reached.

## CUTTING THE GRADUATIONS ON A MICROMETER DIAL

In experimental work or the making of special attachments a micrometer dial is sometimes needed in connection with a screw having a certain pitch and lead. With the pitch and lead known a dial can be accurately graduated with the aid of a Dividing Head and a small tool which is easily made. The following example will be used for the purpose of explaining the setup and operation of the Dividing Head for this particular job.

### **Example:**

PITCH OF SCREW	
LEAD OF SCREW	
DIAMETER OF DIA	

1. Clean milling machine table and bottoms of Dividing Head and tailstock.

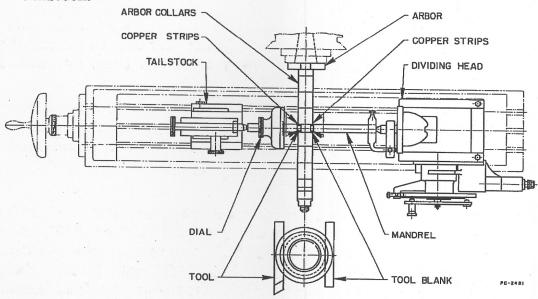


Figure 54
Graduating an Index Dial

### SETTING UP THE DIVIDING HEAD

- 2. Clamp Dividing Head in center T-slot with spindle in a horizontal position. Insert a center in spindle of Dividing Head.
- 3. Align tailstock center with Dividing Head center. Clamp tailstock to table of machine.
- 4. Grind a piece of tool steel to any desired shape which will be easily read when reproduced on the periphery of the dial.
- 5. Fasten arbor with arbor collars into spindle of machine. At a convenient distance from the spindle nose separate two of the arbor collars about 1 inch (Figure 54). Place two thin pieces of copper on each side of tool and mount between separated arbor collars. Similarly place a tool blank, with copper strips, between arbor collars directly opposite tool and tighten arbor nut.
- 6. Manipulate knee, saddle, and table until tool point is in line with tailstock center. Lower knee and set machine to lowest spindle R. P. M. Mount arbor support on overarm and tighten arbor support bushing nut.
- 7. Dog end of mandrel, preferably a flange type. Fasten work piece on mandrel and mount between centers.
- 8. Manipulate knee, saddle, and table until tool point contacts periphery of dial blank. Set the table dogs for desired length of graduated line. Move the table away from tool point by hand. Raise knee for desired depth of graduation line.
- 9. Each graduation is cut by using the longitudinal feed of the machine and indexing the dividing head by means of the hand index crank.

A ¼" pitch and ¼" lead indicates a single thread screw. Therefore one complete turn of dial would advance screw ¼" or .250". It will be necessary therefore to have 250 graduations on periphery of dial. This can be obtained with the dividing head as follows: Set the index crank so pin enters hole in 25-hole circle. Set the sectors four holes apart. After one graduation mark is cut, move index crank to sector arm (4 holes) swing sector arms around for next index.

### MILLING CAMS

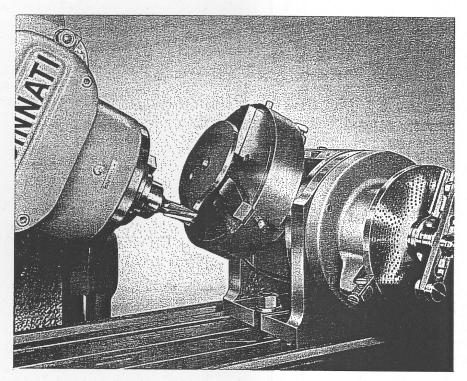


Figure 56
Milling a Uniform Rise Cam

Rise and fall cams having a relatively narrow face may be machined by using the type of setup indicated in Figure 56. The cutter may be supported in any type of swiveling head, such as a Universal Milling Attachment or Vertical Attachment. Almost any cam lead can be machined, and by trying different Dividing Head leads, the angle to which the head must be set can be changed to suit conditions. A table of Sine functions will be required when determining the angle of inclination of the Dividing Head.

The angle of inclination of the Dividing Head and milling cutter can be calculated by means of the following formula.

Sine 
$$A = \frac{\text{Lead of Cam}}{\text{Lead of Dividing Head}}$$

### **Examples:**

1. Suppose you want to mill a cam having a .500" lead. Assume change gears are set up for 2.5" Dividing Head Lead.

Sine 
$$A = \frac{\text{Lead of Cam}}{\text{Lead of Dividing Head}} = \frac{.5}{2.5} = .200 \text{ A} = 11^{\circ}, 33'.$$

### SETTING UP THE DIVIDING HEAD

- 2. Suppose you want to mill a lead of 6.005".
  - (a) Assume change gears are set up for 8" Dividing Head Lead.

Sine 
$$A = \frac{\text{Lead of Cam}}{\text{Lead of Dividing Head}} = \frac{6.005}{8} = .7506$$
  $A = 48^{\circ}$ , 39'.

(b) Assume change gears are set for 9.935" Dividing Head Lead instead of 8" as in example 2 (a), then

Sine 
$$A = \frac{\text{Lead of Cam}}{\text{Lead of Dividing Head}} = \frac{6.005}{9.935} = .6044$$
  $A = 37^{\circ}$ , 11'.

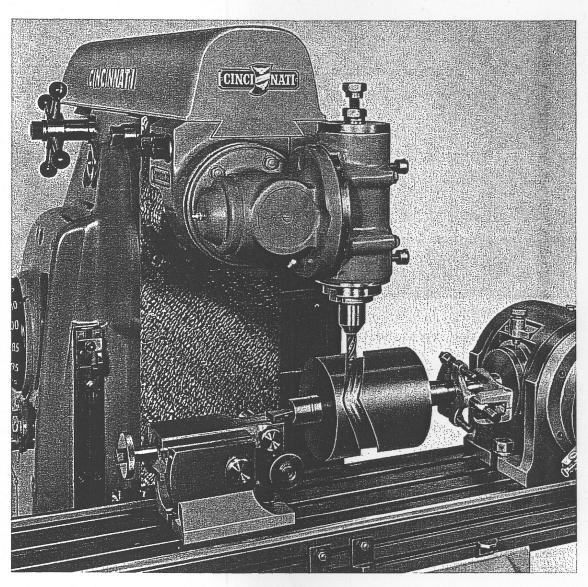


Figure 57
Milling a Reverse Type Drum Cam

### **DRIVING MECHANISMS**

There are three classifications of driving mechanisms for CINCIN-NATI Universal Dividing Heads. Instructions and tables in this book are for the 2½" to 100" Standard Enclosed Driving Mechanism only. The instructions and tables for the Low Lead Attachment and the Short and Long Lead Attachment are contained in separate booklets.

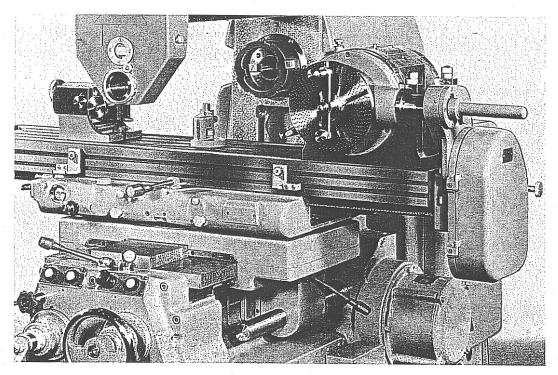


Figure 58  $2\sqrt[4]{2}''$  to 100" Standard Enclosed Driving Mechanism

2½" to 100" Standard Enclosed Driving Mechanism. This driving mechanism is supplied with all CINCINNATI Universal General Purpose Milling Machines as standard equipment (Figure 58). It is available for plain and vertical style machines. The instructions and tables for this attachment are in this book and are also in a separate booklet, "Table of Leads—2½" to 100" Standard Enclosed Driving Mechanism."

Note: There is a  $2\frac{1}{2}$ " to 150" Standard Enclosed Driving Mechanism which is available for all general purpose milling machines (plain, universal, and vertical). The instructions and tables in this book do not apply to this mechanism. Complete information is contained in the booklet, "Table of Leads— $2\frac{1}{2}$ " to 150" Standard Enclosed Driving Mechanism."

Low Lead Attachment. May be obtained at extra cost for the CINPAK® 45, CINEL® 60, and CINOVA® 80 Universal Machines only (Figure 59A). Complimentary parts must be built into the machine at the factory. It is driven from a splined shaft and has a lead range of  $\frac{1}{8}$ " to 100" (high series same as tables on pages 76 to 92; low series are these leads divided by 20). Complete instructions are contained in a separate booklet "Table of Low Leads—1/8" to 100" Dividing Head Driving Mechanism for CINCIN-NATI® Milling Machines," a copy of which accompanies each machine equipped with the Low Lead Attachment.

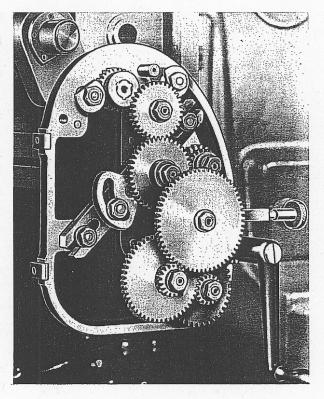


Figure 59A Low Lead Attachment

Short and Long Lead Attachment. May be obtained at extra cost for all CINCINNATI Universal General Purpose Milling Machines (Figure 59B). Complimentary parts must be built into the machine at the factory. It has a standard range of .010" to 1000" or (on demand) .025" to 3000". with no more than the usual number of change gears. Complete instructions are contained in a separate booklet, "Short and Long Lead Attachment-Table of Leads for CIN-CINNATI Universal Milling Machines," a copy of which accompanies each machine equipped with this attachment.

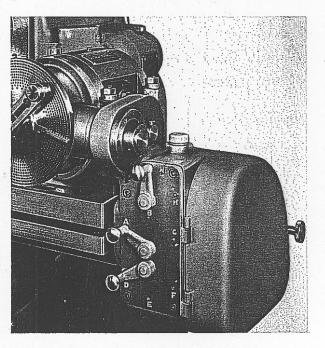


Figure 59B
Short and Long Lead Attachment

# 21/2" TO 100" STANDARD ENCLOSED DRIVING MECHANISM

This Dividing Head driving mechanism is supplied with all CINCIN-NATI Universal General Purpose Milling Machines as standard equipment. It is available for plain and vertical machines. Driven directly from the lead screw, this attachment provides leads from  $2\frac{1}{2}$ " to 100" (See "Tables of Leads", pages 76-92). For illustrations and operating instructions for this driving mechanism only, see pages 60-63.

Note: This driving mechanism is not interchangeable from one size machine to another.

Calculating the Change Gears Required for a Given Lead. Many leads can be obtained other than those listed in the "Table of Leads". They were omitted because the difference was too small for ordinary requirements; but if you do not find a lead in the table which is close enough to meet your needs, the following formula will enable you to calculate all the possibilities:

$$\frac{\text{Lead}}{10} = \frac{\text{Driven Gears}}{\text{Driver Gears}} = \frac{A \times C}{B \times D}$$

Suppose you want a lead of 35.789":

$$\frac{35.789}{10} = 3.5789 = \frac{204}{57} = \frac{51 \times 4}{19 \times 3} = \frac{51 \times (4 \times 9)}{19 \times (3 \times 9)} = \frac{51 \times 36}{19 \times 27}$$

Gear A = 51 teeth Gear C = 36 teeth Gear B = 19 teeth Gear D = 27 teeth

Standard change gears furnished with enclosed driving mechanism:

		0
1 — 17 teeth	2 — 24 teeth	1 — 42 teeth
1 — 18 teeth	1 — 27 teeth	1 - 45 teeth
1 — 19 teeth	1 - 30 teeth	1 — 48 teeth
1 — 20 teeth	1 - 33 teeth	1 — 51 teeth
1 — 21 teeth	1 — 36 teeth	1 — 55 teeth
1 — 22 teeth	1 — 39 teeth	1 — 60 teeth

The "hand" of the lead is fixed by gears "X" and "Y", as shown in the table below:

Right-Hand Helix	Left-Hand Helix
Remove gear Y	Gears X and Y as
Reverse gear X	shown in Fig. 61B.

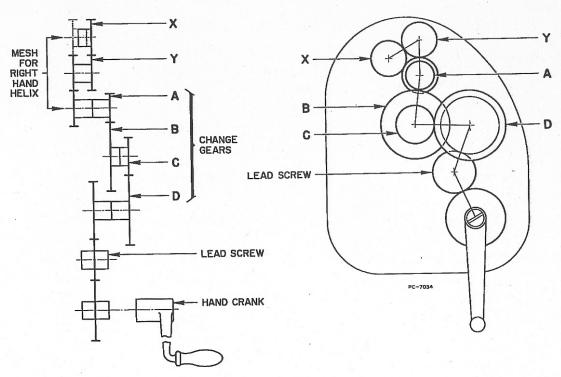


Figure 61A
Arrangement of Change Gears

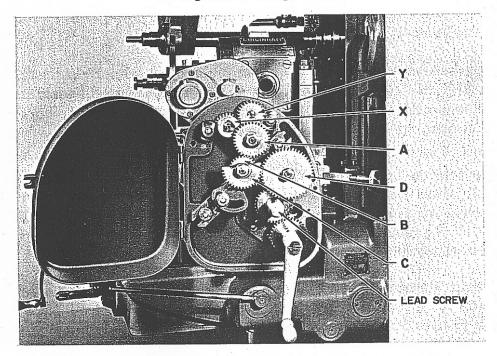


Figure 61B Arrangement of Complete Gear Train

### CINCINNATI UNIVERSAL DIVIDING HEADS

Setting Up the Change Gears. Remove the circular cover on the apron at the right-hand end of the table. It is held in position with a slotted screw. Then place the change gear driving mechanism on the apron, and fasten securely in position. Place the change gears in the positions indicated for the desired lead, being careful not to get intermediate gears B and C interchanged (Figures 61A and 61B).

After the setup has been completed, move the table by means of the hand feed crank, to insure that the entire mechanism operates freely, before engaging the power feed.

Emergency Conversion to Short Leads. With the 2½" to 100" Standard Enclosed Driving Mechanism, illustrated in Figure 61B, leads lower than those listed in the tables, pages 76 to 92, can be obtained, using hand feed only (rotating the index crank at the side of the head). To change the gearing for low leads, remove gear "D". A 34-tooth gear is now exposed, meshing with the 34-tooth gear on the lead screw (directly below gear "D"). Remove these two 34-tooth gears, and replace them with the standard 51-tooth change gear on the lead screw and the standard 17-tooth change gear on the stud for gear "D". Instead of a 1 to 1 ratio, we now have a speed-up of 3 to 1. Leads for the change gear combinations listed are now divided by 3. However, some of the change gear combinations are not obtainable because of interference with the segment.

This setup should be used only for occasional jobs. If leads shorter than  $2\frac{1}{2}$ " are cut often, we recommend the Low Lead Attachment or the Short and Long Lead Attachment. Of course, these short lead mechanisms can be installed only at our factory.

Leads Near the Low Range. When cutting leads within the low range of the Dividing Head driving mechanism, certain precautions must be observed. If, for example, the gears are set up for a 10" lead, the ratio of the change gears is 1 to 1, and the table feed (lead) screw rotates 40 revolutions to one revolution of the Dividing Head spindle.

For leads greater than 10", the Dividing Head spindle runs slower in relation to the speed of the lead screw. Example: 20" lead, table feed screw rotates 80 revolutions, while the Dividing Head spindle rotates one revolution. This requires a change gear setup which reduces the speed from the lead screw to the Dividing Head, resulting in a mechanical advantage in transmitting power.

For leads shorter than 10", the Dividing Head spindle runs faster in relation to the speed of the lead screw. Example: 5" lead, table feed screw rotates 20 revolutions, while the Dividing Head spindle rotates one revolution. The change gear setup for these low leads increases the speed from the lead screw to the Dividing Head, resulting in a mechanical disadvantage in transmitting power. The slow speed of the lead screw causes a "wind-up", which may produce a slightly jerky motion when milling short leads on large diameters of work. Therefore, conditions should be as nearly correct as possible when cutting short leads, particularly those from 21/2" to 5". These conditions may be summarized in a few words: (a) the table gib should be correctly adjusted (not too tight), (b) the change gears should has a slight amount of backlash, (c) the table ways and lead screw should be well oiled, (d) the table feed should rotate freely. Also, it might be noted that with a relatively high table feed, say 53/4" per minute, a greater proportion of power is available at the Dividing Head.

When all contributing factors are correct, the machine will pull a reasonable cut with a setup for the lowest lead of  $2\frac{1}{2}$ ". If the cut should be unnecessarily heavy, then it is advisable to feed by hand. This may be done by allowing the table feed engaging lever to remain in neutral position and driving the Dividing Head and table by hand through the index crank in front of the index plate. With a short lead setup, hand feed is very easy, as the mechanical advantage is then in favor of the operator.

If leads lower than 5" must be cut often, we recommend our short lead attachments. (They may be applied to universal machines only.)

Rapid Traverse and High Feed Rates. When the driving mechanism is set up for low leads, do not engage the table rapid traverse, or use high feed rates of 11" or 16" per minute. Such rapid rates of table traverse drive the Dividing Head too fast, resulting in rapid wear or perhaps "freezing" of the Dividing Head spindle in the block, as they are fitted very closely to obtain accuracy in spacing.

Rapid Traverse. When using the driving mechanism, reverse the table only when the feed is engaged. Do not reverse it while the rapid traverse is engaged, as entirely too much strain is set up in the mechanism of the machine and attachment. For example, after milling a spiral groove, reverse the table while in feed and then engage the rapid traverse to get back to the starting point.

Lubrication. There are three spring cap oilers on the driving mechanism which should be oiled every day with a good quality paraffinic base, rust and oxidation inhibited oil (P-55).

### **ACCESSORIES AND ATTACHMENTS**

### HIGH NUMBER INDEXING PLATES

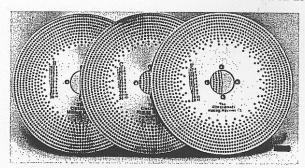


Figure 64
High Number Indexing Plates

This attachment, shown in Figure 64, consists of three plates, drilled on both sides. These plates are interchangeable with the standard index plate on the side of the head.

The index tables shown on pages 74 and 75 apply to this attachment.

### Number of Holes Drilled in Each Side of High Number Index Plates

		Part Numbe	er of Plate					
*Standar †Wide Ran		Standar Wide Rang		Standard 10527 Wide Range 113507				
Side A	Side B	Side C	Side D Side E					
189	199	197	193	191	187			
177	183	181	179	175	173			
171	169	167	163	161	159			
147	157	153	149	143				
129	141	139	137	133	131			
117	127	123	121	119	113			
99	111	109	107	103	101			
91	_ 97	93	89	87	83			
69	81	79	77	73	71			
48	67	46	44	42	38			
30	36	34	32	26	28			

Note: \*Available only for the 10", 12", 14" Universal Dividing Heads. †Available for the 10", 12", 14" Wide Range Dividers.

For leads shorter than 10", the Dividing Head spindle runs faster in relation to the speed of the lead screw. Example: 5" lead, table feed screw rotates 20 revolutions, while the Dividing Head spindle rotates one revolution. The change gear setup for these low leads increases the speed from the lead screw to the Dividing Head, resulting in a mechanical disadvantage in transmitting power. The slow speed of the lead screw causes a "wind-up", which may produce a slightly jerky motion when milling short leads on large diameters of work. Therefore, conditions should be as nearly correct as possible when cutting short leads, particularly those from 2½" to 5". These conditions may be summarized in a few words: (a) the table gib should be correctly adjusted (not too tight), (b) the change gears should has a slight amount of backlash, (c) the table ways and lead screw should be well oiled, (d) the table feed should rotate freely. Also, it might be noted that with a relatively high table feed, say 53/4" per minute, a greater proportion of power is available at the Dividing Head.

When all contributing factors are correct, the machine will pull a reasonable cut with a setup for the lowest lead of  $2\frac{1}{2}$ ". If the cut should be unnecessarily heavy, then it is advisable to feed by hand. This may be done by allowing the table feed engaging lever to remain in neutral position and driving the Dividing Head and table by hand through the index crank in front of the index plate. With a short lead setup, hand feed is very easy, as the mechanical advantage is then in favor of the operator.

If leads lower than 5" must be cut often, we recommend our short lead attachments. (They may be applied to universal machines only.)

Rapid Traverse and High Feed Rates. When the driving mechanism is set up for low leads, do not engage the table rapid traverse, or use high feed rates of 11" or 16" per minute. Such rapid rates of table traverse drive the Dividing Head too fast, resulting in rapid wear or perhaps "freezing" of the Dividing Head spindle in the block, as they are fitted very closely to obtain accuracy in spacing.

Rapid Traverse. When using the driving mechanism, reverse the table only when the feed is engaged. Do not reverse it while the rapid traverse is engaged, as entirely too much strain is set up in the mechanism of the machine and attachment. For example, after milling a spiral groove, reverse the table while in feed and then engage the rapid traverse to get back to the starting point.

Lubrication. There are three spring cap oilers on the driving mechanism which should be oiled every day with a good quality paraffinic base, rust and oxidation inhibited oil (P-55).

### **ACCESSORIES AND ATTACHMENTS**

### HIGH NUMBER INDEXING PLATES

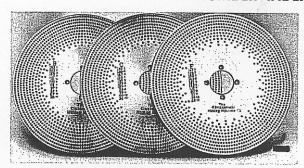


Figure 64
High Number Indexing Plates

This attachment, shown in Figure 64, consists of three plates, drilled on both sides. These plates are interchangeable with the standard index plate on the side of the head.

The index tables shown on pages 74 and 75 apply to this attachment.

### Number of Holes Drilled in Each Side of High Number Index Plates

1		Part Numbe	er of Plate					
*Standar †Wide Ran		Standar Wide Rang		Standard 10527 Wide Range 113507				
Side A	Side B	Side C	Side F					
189	199	197	193	191	187			
177	183	181	179	175	173			
171	169	167	163	161	159			
147	157	153	151	149	143			
129	141	139	133	131				
117	127	123	121	119	113			
99	111	109	107	103	101			
91	. 97	93	89	87	83			
69	81	79	77	73	71			
48	67	46	44	42	38			
30	36	34	32	26	28			

Note: \*Available only for the 10", 12", 14" Universal Dividing Heads. †Available for the 10", 12", 14" Wide Range Dividers.

### ACCESSORIES AND ATTACHMENTS

### COMPENSATING DOG AND DRIVER

The Compensating Dog and Driver, Figure 65 should be used with CINCINNATI Universal Dividing Heads, because the spindle is not fixed in a horizontal plane. With these driving elements, greater accuracy will be obtained on taper work. The tail of the dog has a close fitting roller, which, in turn, fits into the slot of the driver. Various work diameters can be handled, because the roller slides on the tail of the dog a sufficient amount to compensate for the varying difference in the distance from the center of the work to the point of driving contact. The dog has a capacity range from 3/4" to 23/4" diameter for 10", 12" and 14" Dividing Heads.

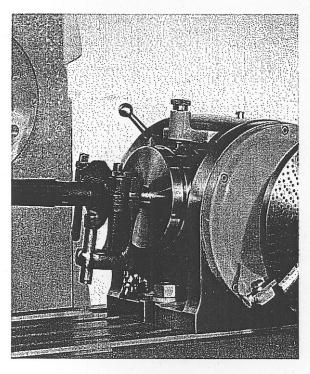


Figure 65
Compensating Dividing Head Dog and Driver

### **CHUCKS**

Many Dividing Head jobs can be more conveniently held in a chuck than between centers. To facilitate this class of work, the 3-Jaw Universal Chuck (Figure 66A) or the 4-Jaw Independent Chuck (Figure 66B) may be obtained.

The chuck bolts to an adapter plate (Figure 66C) designed for the 50 Series spindle nose of the Dividing Head. See specifications (Figure 66D) below for various size chucks and adapters.

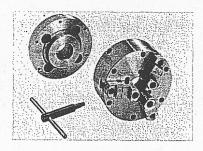


Figure 66A 3-Jaw Universal Chuck, Adapter "A", and T-Wrench

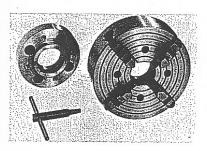
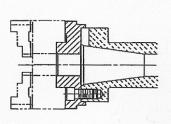
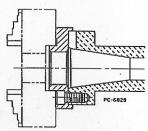


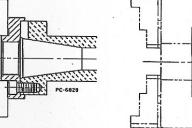
Figure 66B 4-Jaw Independent Chuck, Adapter "B", and T-Wrench



Adapter Style "A"



Adapter Style "B"



Adapter Style "C"

Figure 66C **Chuck Adapters** 

Size Head	Chuck Size	Style	Capacity	Adapter
10"	6" Universal	3-Jaw	½8"-7¾" O.D. 1¾"-5" I.D.	Style A
10"	8" Independent	4-Jaw (light duty)	2½"-7¾" O.D. 2"-7¼" I.D.	Style B
12"-14"	9" Universal	3-Jaw	1/4"-81/2" O.D. 21/4"-81/2" I.D.	Style C
12"-14"	10" Independent	4-Jaw (light duty)	3½"-9½" O.D. 2"-8¼" I.D.	Style B

Figure 66D **Specifications** 

### UNIVERSAL MILLING ATTACHMENT

This attachment is used for helical milling in two cases:

- 1. If the machine is a plain miller, obviously the table can not be swiveled to bring the work piece to the correct helix angle with the cutter. It then becomes necessary to swivel the cutter. This angular setting is obtained by means of the Universal Milling Attachment (Figure 67).
- 2. The table of a universal miller can not be swiveled more than 45°. If the helix angle exceeds this range, the attachment must be used, since it allows the cutter to be swiveled through a complete circle.

The Universal Milling Attachment may also be employed for a wide variety of other types of work, such as vertical milling with a shell end mill, rounding out keyways, milling angular surfaces, etc. The attachment spindle runs at the same speed as the machine spindle.

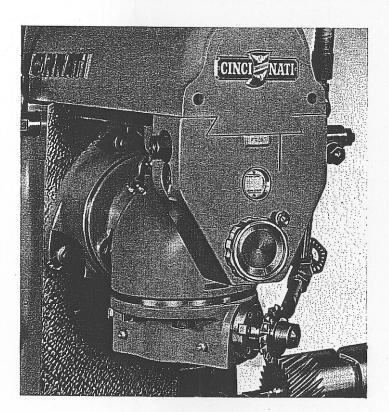


Figure 67
Universal Milling Attachment

# GASHING ANGLES FOR WORM WHEELS

	21/2	444, 449, 544, 10 3, 10 13, 10 13, 10 49, 20 26, 20 25, 40 10, 40 10, 40 50 27, 50 44, 50 27,
	23%	46, 1017, 1032, 1017, 1032
		• • •
	21/4	10 01 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	21.8	104, 1014, 1026, 1026, 1026, 1026, 1043, 1
	2	10 0 15 10 10 10 15 10 10 18 10 18 1
Σ	12%	10 58, 10 13, 10 13, 10 23, 10 24, 20 26, 20 47, 20 32, 20
OF WORM	13/4	10 0 2 10 10 9 10 10 18 10 10 18 10 10 14 10 14 10 14 10 10 18 10 10 10 10 10 10 10 10 10 10 10 10 10 1
	15%	10 7/ 1015/ 1024/ 1052/ 1052/ 2015/ 3012/ 3012/ 4012/ 4012/ 6023/ 6023/
DIAMETER	17%	1013 10211 10311 1044 1044 20 1 20 2 30 2 4033 4033 6055 6055
PITCH D	13,8	1028/ 1028/ 1038/ 1054/ 2013/ 2038/ 8041/ 8041/ 8058/ 6052/ 6052/
ē.	74	1028/ 1037/ 1049/ 2056/ 2056/ 2056/ 5017/ 7015/
grant and	178	1037 10487 2019/2019/2019/2019/2019/2019/2019/2019/
	-	1049 2017 1017 1017 1017 1018 1018 1018 1018 1
	78	20 5/ 2016/ 2038/ 3028/ 4010/ 6055/ 7046/ 8017/
	%	2022 2024 2028 4027 2028 9038 9038 9038
	%	2055/ 3014/ 3038/ 4010/ 4051/ 9038/ 11031/ 11031/
No. of Threads per Inch	in Worm	000000400000000000000000000000000000000
Lead of Worm	in Inches	1,10 1,10 1,10 1,10 1,10 1,10 1,10 1,10

# GASHING ANGLES FOR WORM WHEELS (Continued)

	9		:			:	46,	52,	10 1/	10 6'	lo S'	1013/	1021	1031	1044	20 1'	2017	2026/	30 2/	40 2'	4033/
	53/4					38/	48/	54′	10 3/	10 9/	1011/	1016/	10247	1035/	1049/	20 7/	2023	2032/	3010/	4013/	4045
	51/2		:		:	40,	50,	57'	10 6'	1012/	1015'	1020/	1°28′	1039/	1054/	2013/	2029/	2039,	3019/	4025/	4058
	51/4				35/	42/	52/	10 1/	10 9/	1016/	1018/	1023/	1033/	1044/	1050/	2019/	2036/	2047	3028/	4037	5012'
	rc				36,	<b>\</b> #	55/	10 3	1013/	1020/	1022/	1028/	1037/	1049/	20 5/	2026/	2044	2055/	3030	4051/	5027
Z	434			33/	38,	46/	58,	10 6/	1017/	1024/	1026′	1032/	1042/	1055/	2012/	20337	2053/	30 4/	3050	50 6	6044′
WORM	41/2		: :	35/	40,	46,	10 1/	10 9/	1021/	1028/	1031	1037	1048/	20	2019/	2042	30 2/	3014/	40 3/	5023/	60 4'
ER OF	4%		32/	37/	43,	52′	10 4'	1014/	1°26′	1034/	1037	1043/	1054	20 97	2027/	2052/	3013/	3026/	4017/	5042/	9209
DIAMETER	4		34′	39,	46′	55,	10 8	1018/	1031/	1039/	1043/	1040/	50 5	2017/	2036/	30 27	3025/	3039/	4033/	60 4/	6049
РІТСН D	33,4		36′	42,	48,	58,	1013/	1023/	1037	10 <sup>4</sup> 0/	1049,	1057/	2010	2026/	2047/	3014/	3039/	3053/	4051/	0027	7015/
PI	31/2		39,	45/	52,	10 3/	1018/	1029/	10#	1057	1°57′	20 57	2019	2036/	2059/	3028/	3054/	4010/	5012/	6054	1046
	314		42/	48,	56,	10 1/	1024	1036/	1052	50 5	20 6	2014	2030	2048	3012/	3044	4012/	4020/	5036	70267	So22,
	က		46/	52′	10.1/	1013/	1031	1044	20 2	2013/	2017	2026	2042	30 2	3028	40 3/	4033/	4051/	60 3/	80 3	90 3/
	27/8		<del>.</del>	54′	10 3/	1916/	1035	1049	20 2/	2018	2023/	2032/	2049	3010	3037	4013'	4045	50 4/	6019	8024	:
	234		50′	57,	10 6/	1020	1030	1,54	2013/	2025/	2029	2039/	2057	3019	3047	1025/	1058	2017/	0036	:::::	:
	25/8		52′	0.0	10.97	1023	101	1059	2019	2031	2036	2047/	30.57	32.25	3058	4037	5012	5032	6055	:	:
No. of Threads per Inch	in Worm	01	n so	1~	9	<u>.</u>	- <del></del>	27/2	, m	C1	22/3	27.5		21	7	172	11 80	77.		74.	25%
Lead of Worm	in Inches	1/10	1/8	1/7	1/6	1/5	1/4	7/7		4/11	8/8	2/5	4/6	7.	1/4	2/3	3/4	4/5	;		1/2

TABLE OF IMPORTANT DIMENSIONS OF WORM THREAD PARTS

Width of Thread at Top	0.6708 0.5869 0.5031 0.4192 0.3354 0.2515 0.2236 0.1677 0.1341 0.01118 0.0559 0.0579 0.0335 0.0335 0.0239 0.0239 0.0239
Width of Thread Tool at End	0.6200 0.5425 0.4650 0.3875 0.3100 0.2325 0.1240 0.1240 0.0775 0.0620 0.0620 0.043 0.0443 0.0443 0.0443 0.0344 0.0310 0.0258
Thick- ness of Tooth on Pitch Line	1.0000 0.8750 0.7500 0.6250 0.5000 0.3333 0.2500 0.2500 0.1667 0.1429 0.1250 0.0833 0.0714 0.0625 0.0556 0.0556 0.0556 0.0550
Whole Depth of Tooth	1.3732 1.2015 1.0299 0.8582 0.6856 0.5149 0.4577 0.2289 0.1962 0.1716 0.1716 0.1716 0.1373 0.1144 0.0981 0.0858 0.0687 0.0687 0.0429 0.0429
Depth of Space below Pitch Line	0.7366 0.6445 0.6445 0.6524 0.4603 0.2762 0.2455 0.1053 0.0920 0.0920 0.0920 0.0819 0.0736 0.0736 0.0526 0.0460 0.0460 0.0369 0.0263 0.0263 0.0263
Height of Tooth above Pitch Line	0.6366 0.5570 0.4775 0.3979 0.3183 0.2387 0.2122 0.1592 0.1061 0.0909 0.0796 0.0796 0.0796 0.0796 0.0796 0.0796 0.0796 0.0797 0.0637 0.0354 0.0354 0.0354 0.0354 0.0354 0.0357
Cir. or Linear Pitch, Decimal Equivs.	2.0000 1.7500 1.5000 1.2500 1.0000 0.7500 0.5000 0.2857 0.2857 0.2222 0.2000 0.1429 0.1250 0.1250 0.1000 0.0556
Circular or Linear Pitch, Inches	011111
No. of Threads per In.	747% 26 66 4 4 ro or 8 2 0 0 4 4 8 8

# TABLE OF ANGULAR DIVISIONS Obtainable With Standard Dividing Head and Wide Range Divider (Use 54-hole circle on large plate) DEGREES

Spaces Crank B	447.00 + 447
Turns of	
Esongo C	321 321 321 322 322 322 322 322 322 322
Spaces Crank B	22.27.24.440.2.2.2.2.440.2.2.2.2.440.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2
Turns of Crank B	######################################
гээлдэС	281 282 283 284 284 289 289 289 289 289 289 289 289 289 289
Spaces Crank B	244 244 251 261 271 271 271 272 273 274 275 275 275 275 275 275 275 275
Turns of Crank B	
Degrees	244432 244432 25532 25532 25532 25533 2553
Spaces Crank B	30 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
Turns of Crank B	232222222222222222222222222222222222222
Degrees	201 201 201 201 202 203 200 200 200 201 211 211 211 211 211 211
Spaces Crank B	\$ 443,300 + 487,000 + 487,
Turns of Crank B	222222222222222222222222222222222222222
 es∋ng⊹Cl	161 1653 1653 1653 1658 1658 1670 1771 1771 1774 1774 1775 1774 1775 1776 1776 1777 1777 1777 1777 1777
Spaces Crank B	45.5548 621348 645.35488 645.35488 645.3548 645.
Turns of Crank B	ZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZ
Degrees	1221 1222 1223 1224 1226 1226 1230 1331 1331 1331 1331 1331 1331 1331
Spaces Crank B	8 4 5 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
Turns of Crank B	000000000000000000000000000000000000000
Degrees	882 882 882 883 883 884 887 887 887 887 887 887 887 887 887
Spaces Grank B	\$23.3488.05. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00.00. \$2.00. \$2.00.
Turns of Crank B	<b>ナ44+55555555555555555555555555555555555</b>
БээтдэС	446444444444444444444444444444444444444
Spaces Crank B	071176 071176
Turns of Crank B	
Degrees	45333333333333333333333333333333333333